## EL5224, EL5324, EL5424



#### Data Sheet

## September 23, 2003

## FN7004.2

## 12MHz Rail-to-Rail Buffers + 100mA V<sub>COM</sub> Amplifier



The EL5224, EL5324, and EL5424 feature 8, 10, and 12 low power buffers, respectively, and one high

power output amplifier. They are designed primarily for buffering column driver reference voltages in TFT-LCD applications as well as generation of the V<sub>COM</sub> supply. Each low power buffer features a -3dB bandwidth of 12MHz and features rail-to-rail input/output capability. The high power buffer can drive 100mA and swings to within 2V of each rail.

The 8-channel EL5224 is available in 24-pin LPP and 24-pin HTSSOP packages, the 10-channel EL5324 is available in 32-pin LPP and 28-pin HTSSOP packages, and the 12-channel EL5434 is available in the 32-pin LPP package. They are specified for operation over the full -40°C to +85°C temperature range.

## **Ordering Information**

PART NUMBER	PACKAGE	TAPE & REEL	PKG. DWG. #
EL5224IL	24-Pin LPP		MDP0046
EL5224IL-T7	24-Pin LPP	7"	MDP0046
EL5224IL-T13	24-Pin LPP	13"	MDP0046
EL5224IRE	24-Pin HTSSOP	-	MDP0048
EL5224IRE-T7	24-Pin HTSSOP	7"	MDP0048
EL5224IRE-T13	24-Pin HTSSOP	13"	MDP0048
EL5324IL	32-Pin LPP		MDP0046
EL5324IL-T7	32-Pin LPP	7"	MDP0046
EL5324IL-T13	32-Pin LPP	13"	MDP0046
EL5324IRE	28-Pin HTSSOP	-	MDP0048
EL5324IRE-T7	28-Pin HTSSOP	7"	MDP0048
EL5324IRE-T13	28-Pin HTSSOP	13"	MDP0048
EL5424IL	32-Pin LPP		MDP0046
EL5424IL-T7	32-Pin LPP	7"	MDP0046
EL5424IL-T13	32-Pin LPP	13"	MDP0046

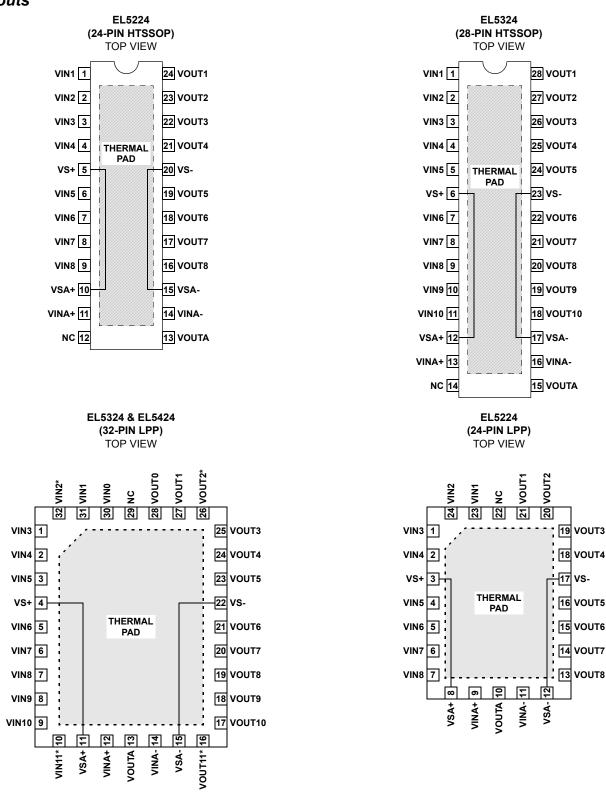
## Features

- 8, 10, and 12 channel versions
- · 12MHz -3dB buffer bandwidth
- 150mA V<sub>COM</sub> buffer
- Operating supply voltage from 4.5V to 16.5V
- · Low supply current 6mA total (8-channel version)
- · Rail-to-rail input/output swing (buffers only)
- LPP package just 0.9mm high

## Applications

- + TFT-LCD column driver buffering and  $\mathsf{V}_{COM}$  supply
- Electronics notebooks
- Computer monitors
- · Electronics games
- · Touch-screen displays
- · Portable instrumentation





\*Not available in EL5324

## Absolute Maximum Ratings $(T_A = 25^{\circ}C)$

Supply Voltage between V <sub>S</sub> + and V <sub>S</sub>	+18V
Input VoltageV <sub>S</sub> 0.5V, V	<sub>S</sub> + +0.5V
Maximum Continuous Output Current (V <sub>OUT0-9</sub> )	30mA
Maximum Continuous Output Current (VOUTA)	. 150mA

 Power Dissipation
 See Curves

 Maximum Die Temperature
 +125°C

 Storage Temperature
 -65°C to +150°C

 Ambient Operating Temperature
 -40°C to +85°C

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

NOTE: All parameters having Min/Max specifications are guaranteed. Typ values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore:  $T_J = T_C = T_A$ 

Electrical Specifications	$V_S$ + = +15V, $V_S$ - = 0, $R_L$ = 10k $\Omega$ , $R_F$ = $R_G$ = 20k $\Omega$ , $C_L$ = 10pF to 0V, Gain of $V_{COM}$ = -1, and $T_A$ = 25°C Unless
	Otherwise Specified

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
INPUT CHARA	CTERISTICS (REFERENCE BUFFER	(S)	1	1		
V <sub>OS</sub>	Input Offset Voltage	V <sub>CM</sub> = 0V		2	14	mV
TCV <sub>OS</sub>	Average Offset Voltage Drift	(Note 1)		5		µV/∘C
Ι <sub>Β</sub>	Input Bias Current	V <sub>CM</sub> = 0V		2	50	nA
R <sub>IN</sub>	Input Impedance			1		GΩ
C <sub>IN</sub>	Input Capacitance			1.35		pF
A <sub>V</sub>	Voltage Gain	$1V \le V_{OUT} \le 14V$	0.992		1.008	V/V
INPUT CHARA	CTERISTICS (V <sub>COM</sub> BUFFER)		IL			
V <sub>OS</sub>	Input Offset Voltage	V <sub>CM</sub> = 7.5V		1	4	mV
TCV <sub>OS</sub>	Average Offset Voltage Drift	(Note 1)		3		µV/∘C
IB	Input Bias Current	V <sub>CM</sub> = 7.5V		2	100	nA
R <sub>IN</sub>	Input Impedance			1		GΩ
C <sub>IN</sub>	Input Capacitance			1.35		pF
V <sub>REG</sub>	Load Regulation	V <sub>COM</sub> = 6V, -100mA < I <sub>L</sub> < 100mA	-20		+20	mV
OUTPUT CHAR	ACTERISTICS (REFERENCE BUFF	ERS)	IL			
V <sub>OL</sub>	Output Swing Low	I <sub>L</sub> = 7.5mA		50	150	mV
V <sub>OH</sub>	Output Swing High	I <sub>L</sub> = 7.5mA	14.85	14.95		V
I <sub>SC</sub>	Short Circuit Current		120	140		mA
OUTPUT CHAR	ACTERISTICS (V <sub>COM</sub> BUFFER)		IL			
V <sub>OL</sub>	Output Swing Low	50Ω to 7.5V		1	1.5	V
V <sub>OH</sub>	Output Swing High	50Ω to 7.5V	13.5	14		V
I <sub>SC</sub>	Short Circuit Current			160		mA
POWER SUPPL	Y PERFORMANCE		IL			
PSRR	Power Supply Rejection Ratio	Reference buffer $V_S$ from 5V to 15V	55	80		dB
		$V_{COM}$ buffer, $V_{S}$ from 5V to 15V	60	100		dB
IS	Total Supply Current	EL5224 (no load)	5	6.8	8	mA
		EL5324 (no load)	6	7.8	9.5	mA
		EL5424 (no load)	7	8.8	11	mA
DYNAMIC PER	FORMANCE (BUFFER AMPLIFIERS	)				
SR	Slew Rate (Note 2)	-4V $\leq$ V_{OUT} $\leq$ 4V, 20% to 80%	7	15		V/µs
t <sub>S</sub>	Settling to +0.1% ( $A_V$ = +1)	$(A_V = +1), V_O = 2V \text{ step}$		250		ns
BW	-3dB Bandwidth	R <sub>L</sub> = 10kΩ, C <sub>L</sub> = 10pF		12		MHz

# **Electrical Specifications** $V_{S}$ + = +15V, $V_{S}$ - = 0, $R_{L}$ = 10k $\Omega$ , $R_{F}$ = $R_{G}$ = 20k $\Omega$ , $C_{L}$ = 10pF to 0V, Gain of $V_{COM}$ = -1, and $T_{A}$ = 25°C Unless Otherwise Specified (Continued)

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
GBWP	Gain-Bandwidth Product	$R_{L} = 10k\Omega, C_{L} = 10pF$		8		MHz
PM	Phase Margin	$R_{L} = 10k\Omega, C_{L} = 10pF$		50		0
CS	Channel Separation	f = 5MHz		75		dB

NOTES:

1. Measured over operating temperature range

2. Slew rate is measured on rising and falling edges

#### **Pin Descriptions**

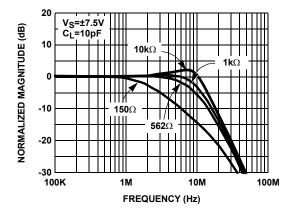
24-PIN HTSSOP	24-PIN LPP	32-PIN LPP	28-PIN HTSSOP	PIN NAME	PIN FUNCTION
1	23	31	1	VIN1	Input
2	24	32 (Note 1)	2	VIN2	Input
3	1	1	3	VIN3	Input
4	2	2	4	VIN4	Input
5	3	4	6	VS+	Power
6	4	3	5	VIN5	Input
7	5	5	7	VIN6	Input
8	6	6	8	VIN7	Input
9	7	7	9	VIN8	Input
10	8	11	12	VSA+	Power
11	9	12	13	VINA+	Positive input of V <sub>COM</sub>
12	22	29	14	NC	Not connected
13	10	13	15	VOUTA	Output of V <sub>COM</sub>
14	11	14	16	VINA-	Negative input of V <sub>COM</sub>
15	12	15	17	VSA-	Power
16	13	19	20	VOUT8	Output
17	14	20	21	VOUT7	Output
18	15	21	22	VOUT6	Output
19	16	23	24	VOUT5	Output
20	17	22	23	VS-	Power
21	18	24	25	VOUT4	Output
22	19	25	26	VOUT3	Output
23	20	26 (Note 1)	27	VOUT2	Output
24	21	27	28	VOUT1	Output
		8	10	VIN9	Input
		9	11	VIN10	Input
		10 (Note 1)		VIN11	Input
		16 (Note 1)		VOUT11	Output
		17	18	VOUT10	Output
		18	19	VOUT9	Output
		28		VOUT0	Output
		30		VIN0	Input

NOTE:

1. Not available in EL5324IL

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## **Typical Performance Curves**





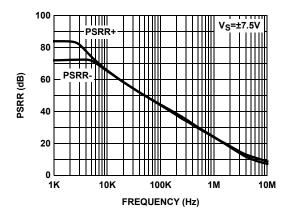


FIGURE 3. PSRR vs FREQUENCY (BUFFER)

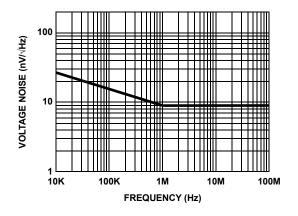


FIGURE 5. INPUT NOISE SPECIAL DENSITY vs FREQUENCY (BUFFER)

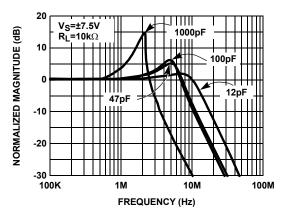


FIGURE 2. FREQUENCY RESPONSE FOR VARIOUS CL (BUFFER)

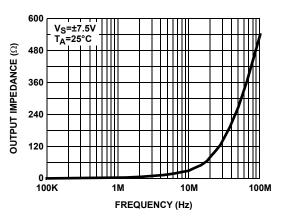


FIGURE 4. OUTPUT IMPEDANCE vs FREQUENCY (BUFFER)

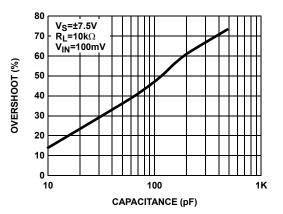


FIGURE 6. OVERSHOOT vs LOAD CAPACITANCE (BUFFER)

## Typical Performance Curves (Continued)

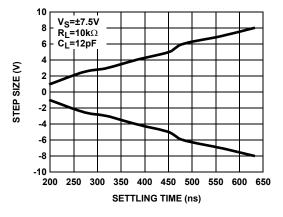


FIGURE 7. SETTLING TIME vs STEP SIZE (BUFFER)

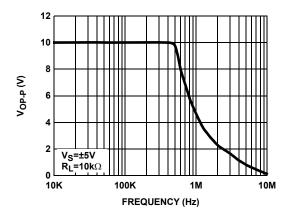


FIGURE 9. OUTPUT SWING vs FREQUENCY (BUFFER)

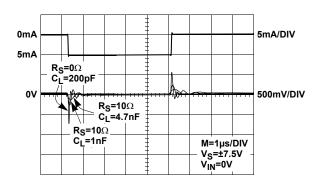


FIGURE 11. TRANSIENT LOAD REGULATION - SOURCING (BUFFER)

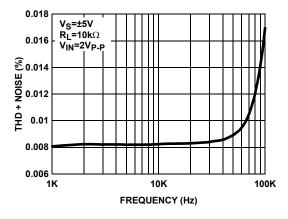


FIGURE 8. TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY (BUFFER)

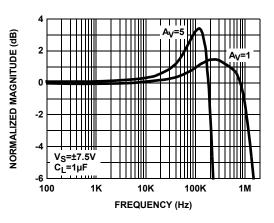


FIGURE 10. FREQUENCY RESPONSE (VCOM)

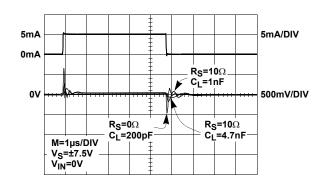
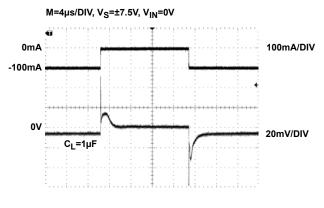
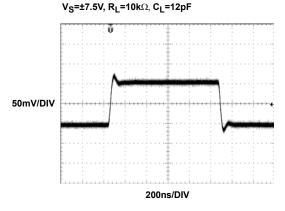


FIGURE 12. TRANSIENT LOAD REGULATION - SINKING (BUFFER)

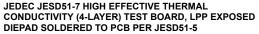
## Typical Performance Curves (Continued)











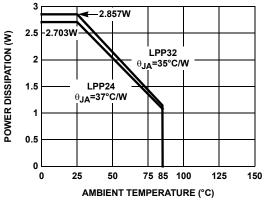


FIGURE 17. PACKAGE POWER DISSIPATION vs AMBIENT TEMPERATURE

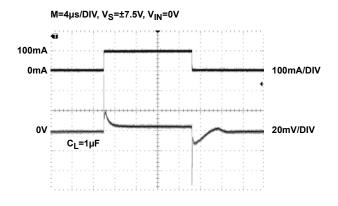
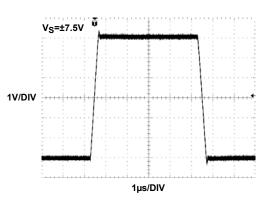
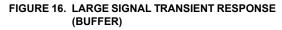
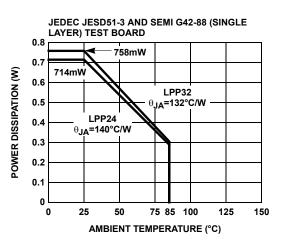


FIGURE 14. TRANSIENT LOAD REGULATION - SINKING (V<sub>COM</sub>)









## Typical Performance Curves (Continued)

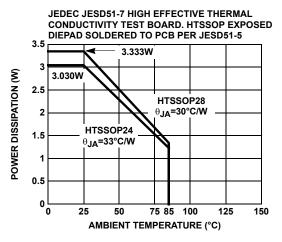


FIGURE 19. PACKAGE POWER DISSIPATION vs AMBIENT TEMPERATURE

## Applications Information

## **Product Description**

The EL5224, EL5324, and EL5424 unity gain buffers and 100mA V<sub>COM</sub> amplifier are fabricated using a high voltage CMOS process. The buffers exhibit rail-to-rail input and output capability and has low power consumption (600µA per buffer). When driving a load of 10k $\Omega$  and 12pF, the buffers have a -3dB bandwidth of 12MHz and exhibits 18V/µs slew rate. The V<sub>COM</sub> amplifier exhibits rail-to-rail input. The output can be driving to within 2V of each supply rail. With a 1µF capacitance load, the GBWP is about 1MHz.

Correct operation is guaranteed for a supply range of 4.5V to 16.5V.

## The Use of the Buffers

The output swings of the buffers typically extend to within 100mV of positive and negative supply rails with load currents of 5mA. Decreasing load currents will extend the output voltage range even closer to the supply rails. Figure 21 shows the input and output waveforms for the device. Operation is from ±5V supply with a 10k $\Omega$  load connected to GND. The input is a 10V<sub>P-P</sub> sinusoid. The output voltage is approximately 9.985V<sub>P-P</sub>.

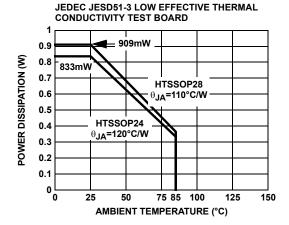


FIGURE 20. PACKAGE POWER DISSIPATION vs AMBIENT TEMPERATURE

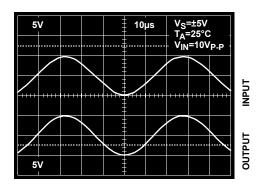


FIGURE 21. OPERATION WITH RAIL-TO-RAIL INPUT AND OUTPUT

## SHORT-CIRCUIT CURRENT LIMIT

The buffers will limit the short circuit current to  $\pm 120$ mA if the output is directly shorted to the positive or the negative supply. If an output is shorted indefinitely, the power dissipation could easily increase such that the device may be damaged. Maximum reliability is maintained if the output continuous current never exceeds  $\pm 30$ mA. This limit is set by the design of the internal metal interconnects.

## **OUTPUT PHASE REVERSAL**

The buffers are immune to phase reversal as long as the input voltage is limited from  $V_{S^-}$  -0.5V to  $V_{S^+}$  +0.5V. Figure 22 shows a photo of the output of the device with the input voltage driven beyond the supply rails. Although the device's output will not change phase, the input's overvoltage should be avoided. If an input voltage exceeds supply voltage by more than 0.6V, electrostatic protection diodes placed in the input stage of the device begin to conduct and overvoltage damage could occur.

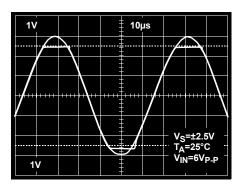


FIGURE 22. OPERATION WITH BEYOND-THE-RAILS INPUT

#### **UNUSED BUFFERS**

It is recommended that any unused buffers have their inputs tied to the ground plane.

#### DRIVING CAPACITIVE LOADS

The buffers can drive a wide range of capacitive loads. As load capacitance increases, however, the -3dB bandwidth of the device will decrease and the peaking increase. The buffers drive 10pF loads in parallel with  $10k\Omega$  with just 1.5dB of peaking, and 100pF with 6.4dB of peaking. If less peaking is desired in these applications, a small series resistor (usually between  $5\Omega$  and  $50\Omega$ ) can be placed in series with the output. However, this will obviously reduce the gain slightly. Another method of reducing peaking is to add a snubber circuit at the output. A snubber is a shunt load consisting of a resistor in series with a capacitor. Values of  $150\Omega$  and 10nF are typical. The advantage of a snubber is that it does not draw any DC load current or reduce the gain.

#### The Use of V<sub>COM</sub> Amplifier

The  $V_{COM}$  amplifier is designed to control the voltage on the back plate of an LCD display. This plate is capacitively coupled to the pixel drive voltage which alternately cycles positive and negative at the line rate for the display. Thus the amplifier must be capable of sourcing and sinking capacitive pulses of current, which can occasionally be quite large (a few 100mA for typical applications).

A simple use of the V<sub>COM</sub> amplifier is as a voltage follower, as illustrated in Figure 23. Here, a voltage, corresponding to the mid-DAC potential, is generated by a resistive divider and buffered by the amplifier. The amplifier's stability is designed to be dominated by the load capacitance, thus for very short duration pulses (< 1µs) the output capacitor supplies the current. For longer pulses the V<sub>COM</sub> amplifier supplies the current. By virtue of its high transconductance which progressively increases as more current is drawn, it can maintain regulation within 5mV as currents up to 100mA are drawn, while consuming only 2mA of quiescent current.

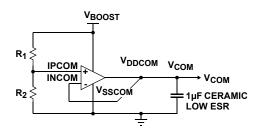


FIGURE 23. V<sub>COM</sub> USED AS A VOLTAGE BUFFER

Alternatively, the back plate potential can be generated by a DAC and the  $V_{COM}$  amplifier used to buffer the DAC voltage, with gain if necessary. This is shown in Figure 24. In this case, the effective transconductance of the feedback is reduced, thus the amplifier will be more stable, but regulation will be degraded by the feedback factor.

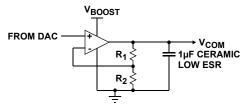


FIGURE 24. V<sub>COM</sub> USED AS A BUFFER WITH GAIN

#### CHOICE OF OUTPUT CAPACITOR

A 1µF ceramic capacitor with low ESR is recommended for this amplifier. (For example, GRM42\_6X7R105K16). This capacitor determines the stability of the amplifier. Reducing it will make the amplifier less stable, and should be avoided. With a 1µF capacitor, the unity gain bandwidth of the amplifier is close to 1MHz when reasonable currents are being drawn. (For lower load currents, the gain and hence bandwidth progressively decreases.) This means the active trans-conductance is:

 $2\pi \times 1 \mu F \times 1 MHz = 6.28S$ 

This high transconductance indicates why it is important to have a low ESR capacitor.

 $ESR \times 6.28 > 1$ 

then the capacitor will not force the gain to roll off below unity, and subsequent poles can affect stability. The recommended capacitor has an ESR of 10m $\Omega$ , but to this must be added the resistance of the board trace between the capacitor and the sense connection - therefore this should be kept short, as illustrated in Figure 21, by the diagonal line to the capacitor. Also ground resistance between the capacitor and the base of R<sub>2</sub> must be kept to a minimum. These constraints should be considered when laying out the PCB. If the capacitor is increased above  $1\mu$ F, stability is generally improved and short pulses of current will cause a smaller "perturbation" on the V<sub>COM</sub> voltage. The speed of response of the amplifier is however degraded as its bandwidth is decreased. At capacitor values around  $10\mu$ F, a subtle interaction with internal DC gain boost circuitry will decrease the phase margin and may give rise to some overshoot in the response. The amplifier will remain stable though.

## **RESPONSE TO HIGH CURRENT SPIKES**

The V<sub>COM</sub> amplifier's output current is limited to 150mA. This limit level, which is roughly the same for sourcing and sinking, is included to maintain reliable operation of the part. It does not necessarily prevent a large temperature rise if the current is maintained. (In this case the whole chip may be shut down by the thermal trip to protect functionality.) If the display occasionally demands current pulses higher than this limit, the reservoir capacitor will provide the excess and the amplifier will top the reservoir capacitor back up once the pulse has stopped. This will happen on the  $\mu$ s time scale in practical systems and for pulses 2 or 3 times the current limit, the V<sub>COM</sub> voltage will have settled again before the next line is processed.

## **Power Dissipation**

With the high-output drive capability of the EL5224, EL5324, and EL5424 buffer, it is possible to exceed the 125°C "absolute-maximum junction temperature" under certain load current conditions. Therefore, it is important to calculate the maximum junction temperature for the application to determine if load conditions need to be modified for the buffer to remain in the safe operating area.

The maximum power dissipation allowed in a package is determined according to:

$$\mathsf{P}_{\mathsf{DMAX}} = \frac{\mathsf{T}_{\mathsf{JMAX}} - \mathsf{T}_{\mathsf{AMAX}}}{\Theta_{\mathsf{JA}}}$$

where:

- T<sub>JMAX</sub> = Maximum junction temperature
- T<sub>AMAX</sub> = Maximum ambient temperature
- θ<sub>JA</sub> = Thermal resistance of the package
- P<sub>DMAX</sub> = Maximum power dissipation in the package

The maximum power dissipation actually produced by an IC is the total quiescent supply current times the total power supply voltage, plus the power in the IC due to the loads, or:

$$\begin{split} \mathsf{P}_{\mathsf{DMAX}} &= \Sigma i \times [\mathsf{V}_\mathsf{S} \times \mathsf{I}_{\mathsf{SMAX}} + (\mathsf{V}_\mathsf{S}^+ - \mathsf{V}_{\mathsf{OUT}}i) \times \mathsf{I}_{\mathsf{LOAD}}i] + \\ [\mathsf{V}_\mathsf{SA} \times \mathsf{I}_\mathsf{SAA} + (\mathsf{V}_\mathsf{SA}^+ - \mathsf{V}_{\mathsf{OUTA}}) \times \mathsf{I}_{\mathsf{LA}}] \end{split}$$

when sourcing, and:

$$\begin{split} \mathsf{P}_{\mathsf{DMAX}} &= \Sigma i \times [\mathsf{V}_{\mathsf{S}} \times \mathsf{I}_{\mathsf{SMAX}} + (\mathsf{V}_{\mathsf{OUT}}i - \mathsf{V}_{\mathsf{S}} \textbf{-}) \times \mathsf{I}_{\mathsf{LOAD}}i] + \\ [\mathsf{V}_{\mathsf{SA}} \times \mathsf{I}_{\mathsf{SAA}} + (\mathsf{V}_{\mathsf{SA}} \textbf{+} - \mathsf{V}_{\mathsf{OUTA}}) \times \mathsf{I}_{\mathsf{LA}}] \end{split}$$

when sinking.

where:

- i = 1 to total number of buffers
- V<sub>S</sub> = Total supply voltage of buffer
- $V_{SA}$  = Total supply voltage of  $V_{COM}$
- I<sub>SMAX</sub> = Maximum quiescent current per channel
- I<sub>SA</sub> = Maximum quiescent current of V<sub>COM</sub>
- V<sub>OUT</sub>i = Maximum output voltage of the application
- V<sub>OUTA</sub> = Maximum output voltage of V<sub>COM</sub>
- ILOADi = Load current of buffer
- I<sub>LA</sub> = Load current of V<sub>COM</sub>

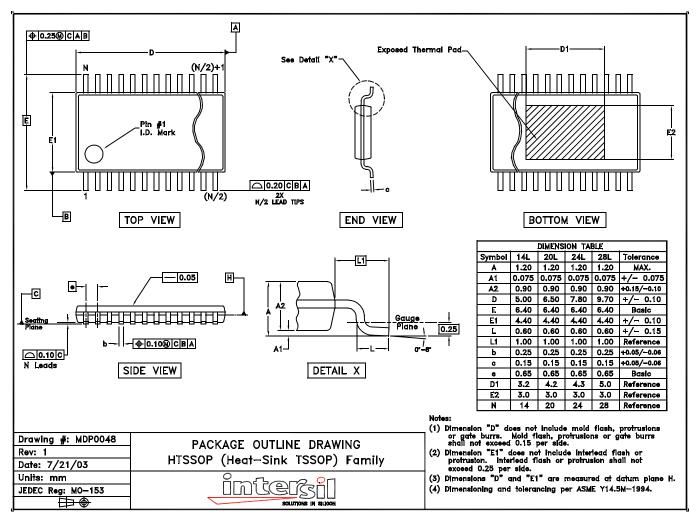
If we set the two  $P_{DMAX}$  equations equal to each other, we can solve for the  $R_{LOAD}$ 's to avoid device overheat. The package power dissipation curves provide a convenient way to see if the device will overheat. The maximum safe power dissipation can be found graphically, based on the package type and the ambient temperature. By using the previous equation, it is a simple matter to see if  $P_{DMAX}$  exceeds the device's power derating curves.

## Power Supply Bypassing and Printed Circuit Board Layout

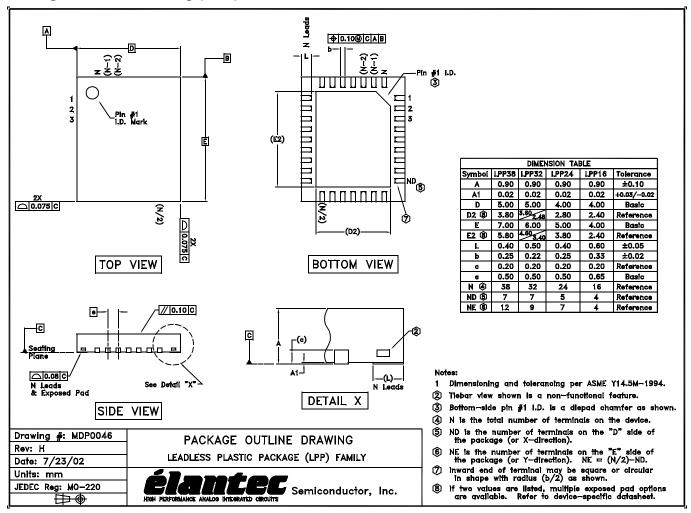
As with any high frequency device, good printed circuit board layout is necessary for optimum performance. Ground plane construction is highly recommended, lead lengths should be as short as possible, and the power supply pins must be well bypassed to reduce the risk of oscillation. For normal single supply operation, where the V<sub>S</sub>- and V<sub>SA</sub>- pins are connected to ground, two 0.1µF ceramic capacitors should be placed from V<sub>S</sub>+ and V<sub>SA</sub>+ pins to ground. A 4.7µF tantalum capacitor should then be connected from  $V_{S}$ + and  $V_{SA}$ + pins to ground. One 4.7µF capacitor may be used for multiple devices. This same capacitor combination should be placed at each supply pin to ground if split supplies are to be used. Internally, V<sub>S</sub>+ and V<sub>SA</sub>+ are shorted together and VS- and VSA- are shorted together. To avoid high current density, the V<sub>S</sub>+ pin and V<sub>SA</sub>+ pin must be shorted in the PCB layout. Also, the V<sub>S</sub>- pin and V<sub>SA</sub>- pin must be shorted in the PCB layout.

Important Note: The metal plane used for heat sinking of the device is electrically connected to the negative supply potential ( $V_{S}$ - and  $V_{SA}$ -). If  $V_{S}$ - and  $V_{SA}$ - are tied to ground, the thermal pad can be connected to ground. Otherwise, the thermal pad must be isolated from any other power planes.

## Package Outline Drawing (HTSSOP)



## Package Outline Drawing (LPP)



NOTE: The package drawings shown here may not be the latest versions. For the latest revisions, please refer to the Intersil website at www.intersil.com/design/packages/elantec

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